## WATERSHED MANAGEMENT ORDINANCE Public Training Session #1

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# SEMINAR OUTLINE

- Introduction to the Watershed Management Ordinance (WMO)
- Differences between the Sewer Permit Ordinance (SPO) and the WMO
- WMO applicability
- New forms and submittal requirements
- Authorized municipalities
- Stormwater management design requirements
- Requirements for flood protection areas (FPAs)
- Resources for stakeholders
- Example stormwater design calculations

# WATERSHED MANAGEMENT ORDINANCE (WMO)

 Replaces the Sewer Permit Ordinance (SPO), which was adopted in 1972

• WMO becomes effective May 1, 2014

 WMO applies to all development within Cook County, except for the City of Chicago (some City of Chicago developments will require District approval)

## SPO VS WMO

### Sewer Permit Ordinance (SPO)

- Sanitary Sewers
- Stormwater Detention
  - TP-40 Rainfall Data
  - Modified Rational Method

### Watershed Management Ordinance (WMO)

- Sanitary Sewers
- Stormwater Detention
  - Bulletin 70 Rainfall Data
  - Flat Release Rate
  - Event Hydrograph Methods
- Volume Control
- Erosion & Sediment Control
- Flood Protection Areas
  - Floodplain
  - Floodway
  - Isolated Wetlands
  - Riparian Environments



# OLD AND NEW PERMIT FORMS

#### • Current Permit Schedules

- Schedule A Project Summary
- Schedule B Sewer Summary
- Schedule C Sewer Connections
- Schedule D Detention
- Schedule E Lift Station / Force Main
- Schedule F Characteristics of Waste Discharge
- Schedule G Treatment / Pretreatment Facilities
- Schedule K Affidavit of Disclosure of Property Interests
- Schedule L Notice of Requirements for Stormwater Detention
- Exhibit A Current Survey of Property Interests

#### New/Revised Permit Schedules

- Schedule D WMO and Schedule D-Legacy Detention
- Schedule H Hazard Areas (Floodplain/Floodway/Riparian)
- Schedule O Outfalls, Direct Connections, District Property
- Schedule P Erosion Control
- Schedule R Recording and Maintenance
- Schedule W Wetlands and Buffer Areas

# DEVELOPMENT/REDEVELOPMENT

#### **Development:**

"Any human-induced activity or change to real estate (including, but not limited to, grading, paving, excavation, dredging, fill, or mining; alteration, subdivision, change in land use or practice; building; or storage of equipment or materials) undertaken by private or public entities that affects the volume, flow rate, drainage pattern or composition of stormwater, or the substantial improvement of an existing building in a Special Flood Hazard Area. The term development shall include redevelopment and shall be understood to not include maintenance."

#### Redevelopment:

"Any human-induced activity or change to an existing <u>developed</u> property (including but not limited to, grading, paving, excavation, dredging, fill, or mining; alteration, subdivision, change in land use or practice; building; or storage of equipment or materials) undertaken by private or public entities that affects the volume, flow rate, drainage pattern, or composition of the site stormwater runoff on the previously developed land. The term shall not be understood to include maintenance."

## WATERSHED MANAGEMENT PERMIT

Permit is required when one of the following is triggered:

- 1) Development is located in a Flood Protection Area (FPA) or causes an indirect wetland impact.
- 2) Development disturbs 0.5 acres or more
- 3) Development proposes drainage improvements in combined sewer area or in conjunction with previously permitted detention facility
- 4) Development involves an outfall to waterway or Lake Michigan
- 5) Development involves sewer or connection to District interceptor or TARP structure

\*Permits for 1 & 2 may be issued by District or authorized municipality. Permits for 3, 4 & 5 can only be issued by District.

### **DEVELOPMENTS EXEMPT FROM WMO PROVISIONS**

- Proposed development was issued Sewerage System Permit before May 1, 2014\*
- A complete Sewerage System Permit application for the proposed development has been accepted by the District prior to May 1, 2014\*
- Development with active Sewerage System Permit issued prior to May 1,2014, but has not been fully constructed by May 1, 2014\*
- 4) Development is on existing development plans list\*
- Development is located within a multi-county municipality that has adopted the other county's ordinance\*\*

\*Must meet standards of Sewer Permit Ordinance (SPO) \*\*Some permits will still be issued by District

### DEVELOPMENTS EXEMPT FROM WMO PROVISIONS

- 6) Agricultural, maintenance, and public utility activities that meet conditions of §201.1.D of the WMO
- 7) Development involves the modification of a septic system, potable water service line, or utility that serves an existing structure
- 8) Development within the City of Chicago, unless it involves:
  - Outfall to waterway or Lake Michigan
  - Stormwater discharges to District property
  - Connections to District sewer, interceptor, or TARP structure
- 9) Development undertaken solely by state or federal agencies (the District, IDOT, Corps, Illinois Tollway Authority, etc.)
- 10) Public flood control projects

## **DEVELOPMENT IN COMBINED SEWER AREA**

- Developments permitted under the Sewer Permit Ordinance (SPO) are not required to provide stormwater detention
- Developments permitted under the WMO must provide both volume control and stormwater detention
  - For volume control practices, underdrains must be 3.5 ft above seasonal groundwater level
  - Detention facilities must be constructed with backflow prevention device
  - Detention facility must be lined if bottom is < 3.5 ft above seasonal groundwater level

### QUALIFICATIONS FOR AUTHORIZED MUNICIPALITIES

For a community to qualify as an authorized municipality, it must meet the following requirements:

- A. Have legal authority to perform all requirements of an authorized municipality as specified in the WMO
- B. Adopt the WMO, including all amendments, by reference
- C. Participate in the National Flood Insurance Program (NFIP)

D. Have the ability to review and issue Watershed Management Permits for development activities in separate sewer areas listed in §201.1 of the WMO and within its corporate boundaries in conformance with the WMO

E. Employ or retain by contract, adequate staff for all of the following positions:

- 1) An enforcement officer
- 2) Professional Engineer(s)
- 3) Wetland specialist(s)
- (continued on next slide)

### QUALIFICATIONS FOR AUTHORIZED MUNICIPALITIES, CONT.

F. Timely review Watershed Management Permit applications and respond within:

- Fifteen (15) working days of an initial submittal for developments not involving flood protection areas (floodplains/wetlands/buffers/riparian environments)
- 2) Thirty (30) working days of an initial submittal for developments involving flood protection areas
- 3) Ten (10) working days of a resubmittal

G. Maintain all of the following records:

- 1) Watershed Management Permits
- 2) Record drawings
- 3) Structure improvement data
- 4) Elevation certificates
- 5) Base flood data and base flood maps
- 6) LOMC, LOMR, etc.

#### (continued on next slide)

### QUALIFICATIONS FOR AUTHORIZED MUNICIPALITIES, CONT.

- H. Transmit all records specified in §1402.2.G of the WMO to the District upon receipt
- I. Issue watershed management permits for development activities listed in §201.1 within its corporate boundaries in conformance with the WMO
- J. Inspect the construction of all developments which require a watershed management permit from the authorized municipality
- K. Notify the District promptly for any violation within the authorized municipality
- L. Issue local stop work orders for all violations, when appropriate
- M. Establish watershed management permit fees for watershed management permits reviewed and issued by the authorized municipality

### AUTHORIZED MUNICIPALITIES

How to become authorized:

 Submit a letter of intent (with supporting documentation) to the District to become an authorized municipality
Template available at: <a href="http://www.mwrd.org/irj/portal/anonymous/managementordinance">http://www.mwrd.org/irj/portal/anonymous/managementordinance</a>

2) Enter into intergovernmental agreement with the District Template available at: <u>http://www.mwrd.org/irj/portal/anonymous/managementordinance</u>

3) Provide contact information for enforcement officer, Professional Engineer, and wetland specialist for the municipality

## AUTHORIZED MUNICIPALITIES

#### Supporting documentation with letter of intent:

- A statement of intent to adopt the WMO by reference
- A legal opinion indicating the authorized municipality has legal authority to perform all obligations required by the WMO including:
  - 1) The regulation of erosion and sediment control, stormwater management, floodplains, isolated wetlands, and riparian environments
  - 2) The ability to conduct inspections
  - 3) The issuance of Watershed Management Permits
  - 4) The enforcement of the WMO
  - 5) The ability to enter into an intergovernmental agreement with the District
- A verified statement of financial capability to perform and adequately fund the obligations of the authorized municipality
- Designation of an enforcement officer
- An implementation plan
- Proposed staffing (enforcement officer, PE, wetland specialist)

## WETLAND SPECIALIST

For a person to qualify as a wetland specialist, he/she must meet the requirements of a), b), c), or d) below:

- a) Certified as an Environmental Scientist in DuPage County or a Certified Wetland Specialist (CWS) in Lake County;
- b) Professional Wetland Scientist certification by the Society of Wetland Scientists (SWS);
- c) Minimum of a bachelor's degree in a biologic science or earth science and at least one of the following:
  - i. Three (3) years cumulative (full-time) wetlands experience in the Upper Midwest Region on wetland-related projects; or
  - ii. Completion of at least 100 wetland delineation projects in the Upper Midwest Region;

d) Six (6) years cumulative (full-time) wetlands experience in the Upper Midwest Region on wetland-related projects without a degree type noted above.

17

## ARTICLE 14 – AUTHORIZED MUNICIPALITIES

Authorized municipalities do <u>not</u> have the authority to issue permits for certain types of projects. The permits must be issued by the District, and the developments include:

- Development that is located within a combined sewer area
- Development that involves modification to the drainage system of a previously permitted detention facility
- Any development that is considered qualified sewer construction
- Development that involves a sewer or connection to District sewer, interceptor, or TARP structure
- Development that involves new or reconstructed outfalls to a waterway\* or Lake Michigan

\*WMO defines waterway as a "navigable body of water such as a stream, creek, canal, or river"

## AUTHORIZED MUNICIPALITIES PERMIT NUMBERING SYSTEM

 When a new application is submitted, the authorized municipality should contact the District to obtain an MWRD permit number for the project. The authorized municipality may adopt its own separate permit numbering system, but the MWRD permit number must be included on all documentation associated with the project

 The MWRD permit number should not be reassigned or consolidated by the Authorized Municipality

### ANNUAL PROJECT STATUS FORM

- The enforcement officer of an authorized municipality must complete an annual project status form for each development permitted by the community.
- The purpose of this form is to provide an inventory of all developments permitted within the authorized municipality, the status of the projects (pre-construction, during construction, and post-construction), as well as the permitting components of the project (stormwater, floodplain, wetland/buffers, and riparian environments).
- The form will be available on-line through the District's website.

#### AUTHORIZED MUNICIPALITY ANNUAL PROJECT STATUS FORM (THIS FORM MUST BE COMPLETED FOR EACH PROJECT)

VUNICIPALITY:		DATE:	
NAME OF DEVELOPMENT:			
DEVELOPMENT ADDRESS:			
TYPE OF DEVELOPMENT (CHEC	ONE BELOW):		
SINGLE FAMILY HOME	RESIDENTIAL SUBDIVISION	MULTI-FAMILY RESIDENTIAL	
□ NON-RESIDENTIAL	RIGHT-OF-WAY	OPEN SPACE	
CHECK COMPONENTS THAT AF	ECT PROJECT:		
STORMWATER	OODPLAIN 🗆 WETLANDS/BUFF	ERS 🗌 RIPARIAN ENVIRONMENT	
CHECK PHASE OF CONSTRUCTION	DN:		
PRE-CONSTRUCTION	DURING CONSTRUCTION	□ POST-CONSTRUCTION	
DESCRIBE TASKS COMPLETED D	URING YEAR:		
I HEREBY CERTIFY THAT ALL T MANAGEMENT ORDINANCE, AI BEST OF MY KNOWLEDGE.	ASKS COMPLETED DURING THIS YE	AR COMPLY WITH THE WATERSHED	
NAME OF ENFORCEMENT OFFI SIGNATURE OF ENFORCEMENT ADDRESS:	CER: OFFICER:FAX NUMBER		
*A COPY OF WATERSHED M	ANAGEMENT PERMIT APPLICATION SHA	LL BE INCLUDED WITH THIS FORM	

## ARTICLE 14 – DISTRICT OVERSIGHT

The District can inspect any development within an authorized municipality, and can, at any time, audit an authorized municipality. During an audit, the District may:

- Inspect and copy pertinent records kept by an authorized municipality
- Inspect Watershed Management Permits issued by an authorized municipality
- Meet with staff of an authorized municipality
- Conduct field inspections of developments permitted by an authorized municipality
- Request and copy financial records of the authorized municipality
- Verify that an authorized municipality complies with all requirements listed in §1402.2 of the WMO
- Verify that an authorized municipality does not violate any provision listed in §1402.3 of the WMO

## MULTI-COUNTY MUNICIPALITIES

- The WMO provides the option for multi-county municipalities to adopt and enforce the adjacent county's stormwater ordinance
- Municipality must enter into IGA with the District
- Certain development activities would still require a Watershed Management Permit from the District (same as authorized municipalities)

# WMO PERMIT SUBMITTAL FLOW CHART



Table 2.			
Summary of Site Stormwater Management Requirements*			
Development Type (See Appendix A for definitions)	Runoff Requirements	Volume Control Requirements	Storage Requirements
Single-Family Home	Exempt	Exempt	Exempt
	Parcels	Parcels	Parcels
Residential Subdivision	≥	≥	≥
	1 acre	1 acre	5 acres
	Parcels	Parcels	Parcels
Multi-Family Residential	≥	≥	≥
	0.5 acre	0.5 acre	3 acres ‡
	Parcels	Parcels	Parcels
Non-Residential	≥	≥	≥
	0.5 acre	0.5 acre	3 acres ‡
	New	New	New
	Impervious	Impervious	Impervious
Right-of-Way	Area	Area	Area
	≥	≥	≥
	1 acre	1 acre †	1 acre †
	Parcels		
Open Space	≥	Not Applicable	Not Applicable
	0.5 acre		

\* Site stormwater management requirements are not required for maintenance activities as defined in Appendix A.

+ Where practicable.

Starting the effective date of this ordinance, any new development on the parcel that totals either individually or in the aggregate to more than one-half (0.5) of an acre.

## WHEN IS VOLUME CONTROL REQUIRED?

## WHEN IS DETENTION REQUIRED?

CHECK TABLE 2 IN WMO...OWNERSHIP AREA STILL USED AS DETERMINING FACTOR

## ARTICLE 3 – STORMWATER MANAGEMENT REQUIREMENTS FLOWCHART



STORMWATER MANAGEMENT REQUIREMENTS FOR REDEVELOPMENT FLOW CHART



## MINOR STORMWATER SYSTEM DESIGN

- Rational Method in conjunction with Intensity-Duration-Frequency (IDF) curves based on Bulletin 70 sectional rainfall depths
- Select land use values for runoff coefficients

Surface Type	Runoff Coefficient, C
Native Plantings	0.15
Pervious Area	0.45
Gravel (loose, unbound)	0.75
Wetlands	0.79
Impervious area (Roads, roofs, sidewalks, etc.)	0.90
Water Surface (open water)	1.00
Green Infrastructure:	
Bioswale	0.15
Rain Garden	0.15
Pervious Surfaces (Porous Asphalt, Pervious Concrete, Permeable Pavers)	0.75

## MAJOR STORMWATER SYSTEM DESIGN

- Event Hydrograph Method
  - HEC-1, HEC-HMS, or TR-20
  - Critical Duration Analysis
  - CN and t<sub>c</sub> calculated using SCS (NRCS) methodology
  - Assume fully developed conditions
  - Design for peak 100-year flowrate
  - Only two Manning's n values for overland flow routes

Surface Type	Manning's n Value	
Paved Channels (asphalt or concrete roadways)	0.013	
Unpaved Channels (grassed)	0.035	

## CALCULATION OF RUNOFF CURVE NUMBER (CN)

#### Land use values will be limited to the following table:

Cover Type and Hydrologic Conditions	Curve Numbers for Hydrologic Soil Group	
	С	D
Native Plantings	70	75
Pervious area (open space, mostly grassed areas)	74	80
Gravel (railroad yards, roads, parking lots)	89	91
Newly graded areas (pervious areas only, no vegetation)	91	94
Wetlands	91	94
Impervious area (roads, roofs, sidewalks, etc.)	98	98
Water surface (open water)	100	100
Green Infrastructure:		
Bioswale	63	70
Rain Garden	63	70
Pervious Surfaces (Porous Asphalt, Pervious Concrete Permeable Pavers)	91	91

## CALCULATION OF TIME OF CONCENTRATION

Using NRCS Methodology, Time of Concentration (t<sub>c</sub>) is combination of:

(1) Sheet Flow:

 $T_{t} = \frac{0.007(nL)^{0.8}}{(P_{2})^{0.5}S^{0.4}}$ 

Overton and Meadows Equation Maximum length = 100 ft

(2) Shallow Concentrated Flow:

$$T_t = \frac{L}{3600V}$$

V is calculated based on paved or unpaved surface

(3) Open Channel Flow:

$$T_t = \frac{L}{3600V}$$

V is calculated using Manning's equation, assuming bankfull conditions

# **VOLUME CONTROL**

- One inch of volume over total impervious area
- Can be provided in several ways:
  - Infiltration Trenches
  - Infiltration Basins
  - Porous Pavement (storage in the voids below the pavement)
  - Bio-Retention Systems
  - Dry Wells
  - Cisterns
  - Open Channel Practices Fitted With Check Dams
  - Storage Below the Outlet of a Site Detention Facility
- Credit toward required detention volume (CN reduction)

## **VOLUME CONTROL DESIGN**

- When providing storage in void space of aggregate, stone must be angular cut and cleaned/washed free of fines. Different aggregate sizes are acceptable
- Underdrains are required, must be offset at least 2" from bottom of volume control storage
- Bottom of storage must be 3.5 ft above seasonal groundwater level in combined sewer areas, 2 feet in separate sewer areas
  Groundwater level established through soil borings
- One monitoring well per 40,000 ft<sup>2</sup> of area

# **FLOW-THROUGH PRACTICES**

- Required for portion of volume control not being provided by volume control practices
- Common flow-through practices are:
  - Vegetated Filter Strips
  - Bio Swales
  - Constructed Wetlands
  - Catch Basin Inserts
  - Oil and Grit Separators

No stormwater detention volume credit for flow-through practices

# VOLUME CONTROL STORAGE CREDIT (CN REDUCTION)

Reduction in composite CN for determining required detention volume

RUNOFF CURVE NUMBER ADJUSTMENT CALCULATOR			
Site Information:			
Total Site Area, A <sub>w</sub> (ac) =	10		Total Impervious Area, A <sub>t</sub> (ac) = 3
Runoff, R (in) =	5.00		
P = rainfall depth (in) =	7.58		
CN =	78		
s =	2.82		
Runoff Volume Over Watershed, V <sub>w</sub> (ac-ft) =	4.17	-	
Volume of GI Provided:			
Control Volume, V <sub>R</sub> =	0.25	ac-ft	1" of volume over impervious area
Additional Volume, V <sub>GI</sub> =	0.00	ac-ft	Additional volume over the required 1"
Adjusted Volume Over Watershed, $V_{ADJ} = V_W \cdot V_R \cdot V_{GI}$			
V <sub>ADJ</sub> (ac-ft) =	3.92		
Adjusted Runoff Over Watershed, $R_{ADJ} = V_{ADJ}$			
R <sub>ADJ</sub> (in) =	4.70		
S <sub>ADJ</sub> =	3.28		
Adjusted CN for detention calcs, CN <sub>ADJ</sub> =	75.32		

# **CN REDUCTION METHODOLOGY**

- Reduce overall runoff volume of the site by the volume provided in retention-based volume control practices
- Use NRCS runoff equation to calculate CN that translates to adjusted runoff volume
- Adjusted CN is used in stormwater detention calculations
- Applicants will use spreadsheet that computes adjusted CN

# **CN REDUCTION METHODOLOGY**

#### Start with selection of CN for developed site:

Cover Type and Hydrologic Conditions	Curve Numbers for Hydrologic Soil Group	
	С	D
Native Plantings	70	75
Pervious area (open space, mostly grassed areas)	74	80
Gravel (railroad yards, roads, parking lots)	89	91
Newly graded areas (pervious areas only, no vegetation)	91	94
Wetlands	91	94
Impervious area (roads, roofs, sidewalks, etc.)	98	98
Water surface (open water)	100	100
Green Infrastructure:		
Bioswale	63	70
Rain Garden	63	70
Pervious Surfaces (Porous Asphalt, Pervious Concrete Permeable Pavers)	91	91
## **CN REDUCTION METHODOLOGY**

The NRCS Runoff Curve Number (CN) method is described in detail in the National Engineering Handbook (NEH-10). The NRCS runoff equation is:

$$R_{\rm W} = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$
 1.0

where,

- $R_W$  = runoff depth (in) from Area,  $A_W$
- P = rainfall depth used to calculate runoff (in),
- S = potential maximum retention after runoff begins (in), and is calculated by:

$$S = \frac{1000}{CN_W} - 10$$
 1.1

where,

CN<sub>W</sub> = composite runoff curve number for the watershed to be developed

The volume of runoff (acre-feet),  $V_W$ , from watershed  $A_W$  (acres) can then be calculated by:

$$V_{\rm W} = A_{\rm w} \times \frac{R_{\rm W}}{12}$$
 1.2

# **CN REDUCTION METHODOLOGY**

The total volume of runoff from the site can be reduced by the volume control required and the extra green infrastructure volume that may be provided:

$$V_{ADJ} = V_W - V_R - V_{GI}$$
 1.3

where,

V<sub>ADJ</sub> = adjusted runoff volume from site (acre-feet)
 V<sub>R</sub>= volume of control volume (1" over impervious area of development)
 V<sub>GI</sub> = volume of green infrastructure provided in addition to the required 1"

This reduced volume of runoff can be reflected in an overall reduction to the CN used in detention basin sizing by using:

$$12 \times \frac{V_{ADJ}}{A_W} = R_{ADJ} = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$
 1.4

Since we know  $R_{ADJ}$ , and we know that P = 7.58" for the 100-year, 24-hour storm event, we can solve for S, which then translates to the adjusted CN.

## **CN REDUCTION EXAMPLE**

#### Example 1

For a 10-acre proposed residential area with a developed CN of 78, and 3 acres of impervious area, find the revised CN resulting from the 1" volume control provisions of the WMO.

The future 100-year runoff volume for the proposed development without volume control can be calculated using equation 1.0 and 1.1.

$$R_{\rm W} = \frac{(7.58"-0.2S)^2}{(7.58+0.8S)}$$

$$S = \frac{1000}{78} - 10 = 2.82^{\circ}$$

$$\mathsf{R}_{\mathsf{W}} = \frac{(7.58" - (0.2)(2.82"))^2}{7.58" + 0.8(2.82")}$$

## **CN REDUCTION EXAMPLE**

The total volume is therefore:

$$V_{W} = \frac{R_{W}}{12} \times A_{W} = \frac{5}{12} \times 10 \text{ acres} = 4.17 \text{ acre-feet}$$

The volume associated with the total impervious area that must be stored is:

$$V_R = 3 \text{ acres} x \frac{1^n}{12} = 0.25 \text{ acre feet}$$

For this example,  $V_{GI}=0$ , so using Equation 1.3:

 $V_{ADJ}$  = 4.17 acre-feet – 0.25 acre feet = 3.92 acre-feet

And using Equation 1.4:

$$12 \times \frac{V_{ADJ}}{A_W} = \frac{(P - 0.2S)^2}{(P + 0.8S)} = 4.70"$$

## **CN REDUCTION EXAMPLE**

Since P=7.58":

4.70 inches =  $\frac{(7.58"-0.2S)^2}{(7.58"+0.8S)}$ 

Solving this equation iteratively:

S = <u>3.28</u>

And from Equation 1.1

CN = <u>75.32</u>

The curve number is reduced from 78 to 75.32. This procedure reflects the stormwater volume reduction and allows for hydrologic routing through proposed stormwater management facilities.

To simplify this procedure, an Excel spreadsheet (next slide) has been provided which reflects the analysis described in this memorandum. The applicant would only have to provide areas, developed CN and the depth of storage being provided. The equation would be solved for the user.

## CN REDUCTION CALCULATOR

RUNOFF CURVE NUMBER ADJUSTMENT CALCULATOR	
Site Information:	
Total Site Area, A <sub>w</sub> (ac) = 10 Total Im	pervious Area, A <sub>i</sub> (ac) = 3
Runoff, R (in) = 5.00	
P = rainfall depth (in) = 7.58	
CN = 78	
s = 2.82	
Runoff Volume Over Watershed, V <sub>w</sub> (ac-ft) = 4.17	
Volume of GI Provided:	
Control Volume, V <sub>R</sub> = 0.25 ac-ft 1" of volume over im	pervious area
Additional Volume, V <sub>GI</sub> = 0.00 ac-ft Additional volume or	ver the required 1"
Adjusted Volume Over Watershed, V <sub>ADJ =</sub> V <sub>W -</sub> V <sub>R -</sub> V <sub>GI</sub>	
V <sub>AD</sub> (ac-ft) = 3.92	
Adjusted Runoff Over Watershed, $R_{ADJ} = V_{ADJ}$	
R <sub>ADJ</sub> (in) = 4.70	
S <sub>ADJ</sub> = 3.28	
Adjusted CN for detention calcs, CN <sub>ADJ</sub> = 75.32	
*Blue values are entered by user	

## **REQUIRED DETENTION VOLUME**

- Determined using event hydrograph method\*
  - HEC-1, HEC-HMS, or TR-20
  - Reduced CN for site based on provided volume control storage
  - Allowable release rate of 0.30 cfs/acre
    - Account for depressional storage and unrestricted releases
  - 100-Year, 24-Hour Rainfall Depth of 7.58"
  - Antecedent Moisture Condition (AMC) of II
  - Tailwater elevation of receiving stream
    - 100-Year flood elevation or HGL

\*Simple sites may use detention nomograph

## UNRESTRICTED RELEASES

Can be handled in three ways:

1) Divert equivalent undetained upstream tributary area

2) Reduce allowable release rate by 100-year, 24-hour flowrate of unrestricted area

Determined using event hydrograph method

3) Plant the unrestricted flow area with deep-rooted vegetation approved by the District or authorized municipality

Allowable release rate based on tributary area to detention facility

## **BYPASS FLOWS**

Recommended design guidance:

Upstream tributary area ≤ 5:1 of the development area
 → Bypass flow through weir of detention facility

Upstream tributary area is ≥ 5:1 of the development area
 → Bypass flow around detention facility

## DETENTION VOLUME NOMOGRAPH

May be used instead of event hydrograph method for simple sites, where:

- The allowable release rate is not affected by existing on-site depressional storage.
- The allowable release rate is not affected by any unrestricted flow.
- There is no upstream tributary flow to the proposed detention facility.
- There are no tailwater conditions on the proposed detention facility's outlet control structure.
- The development provides the required volume control storage (one inch).

## DETENTION VOLUME NOMOGRAPH



Detention volume as a function of reduced CN allows flexibility with varying amounts of volume control storage provided.

#### FLOODPLAIN REQUIREMENTS

 Allowable flood elevation increases of 0.1 ft and velocity increases of 10%

Compensatory storage required at 1.1:1 ratio

- Must use average end method
- 0-10 Year Increment may be provided at 1:1
- 10-100 Year Increment may be provided at 1:1
- 0-100 Year Increment must be provided at 1.1:1
- Flood Protection Elevation (FPE)
  - Two feet above BFE (from FIS or project-specific study)
  - New buildings in floodplain must be elevated by fill to the FPE
    - No basement without a LOMR-F
  - New buildings outside of floodplain must have window wells/perimeter berm elevated to FPE

#### FLOODWAY REQUIREMENTS

Follows IDNR-OWR Part 3708 Rules and Appropriate Uses

• Hyperlinks to IDNR-OWR forms and guidance:

- Joint application form
- Part 3700 & 3708 rules
- Statewide and General Permit information

 Guidance on processes to designate/re-designate a regulatory floodway

#### WMO WETLAND REGULATIONS

WMO regulates direct and indirect impacts to isolated wetlands

The WMO does <u>not</u> regulate Corps jurisdictional wetlands

 District or authorized municipality must receive copies of all Corps correspondence

#### WETLAND DELINEATION GUIDANCE

 Wetland delineation based on USACE Manual (<u>Regional</u> <u>Supplement to the USACE Wetland Delineation Manual:</u> <u>Midwest Region</u>)

Hyperlink to USACE Manual provided in TGM

 Farmed wetlands delineated using the <u>National Food</u> <u>Security Act Manual (NFSAM)</u>

- Otherwise known as the "Swamp Buster Act"
- Hyperlink to NFSAM Manual provided in TGM

 TGM provides examples of exempt wetlands (roadside ditches, incomplete construction, detention basins, etc.)

### **ISOLATED WETLAND CLASSIFICATION**

#### Classified as either "High Quality" or "Standard"

Hyperlink to USACE Manual provided in TGM

#### "High Quality" if one or more of these criteria is met:

- Swink and Wilhelm Floristic Quality Index (FQI) value greater than or equal to 20 during a single season assessment, or a native mean C-value of 3.5 or higher
- Wetland is a habitat for a state-listed threatened or endangered species

#### • Define buffers based on classification:

Wetland Quality	Acreage	Buffer Width (ft)		(ft)
Wetland QualityAcreageStandard Isolated Wetland≥0.1 to < 0.5 acrHigh Quality Isolated Wetland>0.5 acre	≥0.1 to < 0.5 acre	30 ft.		
	≥ 0.5 acre		50 ft	
High Quality Isolated Wetland	No minimum			100 ft

#### IMPACTS TO ISOLATED WETLANDS

- Impacts to high quality and standard isolated wetlands
  - Practicable Alternatives Analysis or hazardous road condition for high quality isolated wetlands
  - Impacts to standard isolated wetlands < 0.1 ac > OK
  - Impacts to standard isolated wetlands ≥ 0.1 ac → Mitigation
  - TGM references federal guidance (USEPA):
    - Memorandum: Appropriate Level of Analysis Required for Evaluating Compliance with the Section 404(b)(1) Guidelines Alternatives Requirements
  - Addresses indirect impacts and acceptable changes to wetland hydrology (80% - 150% for 2-year, 24-hour storm event)

### **ISOLATED WETLAND MITIGATION**

-	Table 5. Isolated Wetland Mitigat	ion Require	ement Ratio	S	
Wetland Quality	Area	§604.9(A)	§604.9(B)	§604.9(C)	§604.9(D)
Standard	<0.10 acre	None			
Isolated Wetland	≥0.10 acre		1.5:1		
High Quality Isolated Wetland	Any			3:1	
Impacts Pri	or to Issuance of Permit				3:1

## **DETENTION IN WETLANDS**

- Detention facilities allowed in standard isolated wetlands
- Not allowed in high quality isolated wetlands
- Allowed in Corps jurisdictional wetlands only if approved by Corps

#### **RIPARIAN ENVIRONMENT**

- Goal is to protect riparian environments that provide functional value
  - TGM makes distinction between areas adjacent to stream that provide a riparian environment function from those that do not
- TGM provides guidance on identifying limits of riparian environment
  - Biological Stream Characterization (BSC) of "A" or "B" (100 feet from OHWM)
  - Biologically Significant Stream (BSS) (100 feet from OHWM)
  - Jurisdictional Waters of the US (50 feet from OHWM)
- Examples of exempt riparian environments
- Guidance on mitigation for riparian environment impacts

## MWRD WMO WEBSITE

- On-line resources include:
- Answers to FAQs
- Authorized Municipalities Documents
- Technical Guidance Manual (TGM)
- Presentations from WMO Advisory Committee meetings and public trainings
- Stormwater calculation spreadsheets
- Template hydrologic models (TR-20, Win TR-20, and HEC-HMS)

## MWRD WMO WEBSITE

<del>(</del> )	https://www.	mwrd.org/irj/p	ortal/anonymous 🔎 🗕 🖒	MWRDGC Porta	al ×								<b>↑</b> ★ ☆
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	(Touge)					enter Ante		R					
Home	Commissioners	Departments	s Services & Facilities	Public Affairs N	lewsroom Bu	usiness with Us	Reports E	mployment					
Cook Cour Plan (CCSI Natershe	nty Stormwater Manag MP) ad Management Ordi	ement	avices & Facilities >> Stormwater Watershed Manager	Management >> Watershi ment Ordinanc	ed Management Ord	linance (WMO)							
nundatior 3tormwate Jublicatior Natershec NPC Meet 2ombined	n Maps & Hydraulic Pro er Annual Reports and sa I Planning Council ings Sewer Communities	files	The Watershed Managen Components which are r environment protection, on October 3, 2013, whi Watershed Management The District is developing through the link below. Draft Technical Guidance The District will conduct Training Schedule Other Resources Watershed Management Authorized Municipalities Multi-County Municipalities	nent Ordinance (W egulated under the and soil erosion ai ch will become effe <u>Ordinance</u> g a Technical Guida a Manual (TGM) training for stakeh <u>Ordinance: Short</u>	(MO) establish a WMO include nd sediment c sective on May ance Manual (` nolders in early <u>Summary</u>	es uniform, mi a drainage and ontrol. The Disf 1, 2014. The V TGM), which wi	nimum, county detention, volu trict's Board of VMO is accessi ill serve as a to ill serve as a to the transition	ywide storm lume control, f Commission ible through echnical refe	water manage floodplain m ners adopted the link below erence to the W wer Permit Or	ment regulat inagement, is the Watershe VMO. The dra dinance to th	ions throughou solated wetland d Management aft TGM docum e WMO.	it Cook C d protecti C Ordinan	ounty. on, riparian ce (WMO) accessible
		1	Existing Development Pl	ans List									
		1	Frequently Asked Questi	ons (FAQs)									
		1	Presentations										
		-	WMO Advisory Committe	ee Resource Page									
		i	If you have any question	ns about the WMO,	contact Mr. Jo	ohn Murray at (	(312) 75 <mark>1-7</mark> 91	18 or <u>john.m</u>	urray@mwrd.	org.			
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https://www.mwrd.org/irj/portal/anonymous/managementordinance

# TGM CONTENTS

- Article 2 Applicability and General Provisions
- Article 3 Watershed Management Permit Requirements and Submittals
- Article 4 Erosion and Sediment Control Requirements
- Article 5 Requirements for Stormwater Management
- Article 6 Requirements for Flood Protection Areas
- Article 7 Requirements for Sewer Construction
- Article 9 Maintenance
- Article 10 Inspections
- Article 14 Administration
- Appendices

## DETENTION VOLUME EXAMPLE PROBLEMS (FROM ARTICLE 5 OF TGM)

- Example 5.7 Simple (Detention Nomograph)
- Example 5.8 Offsite and Unrestricted Areas (HEC-HMS)
- Example 5.9 Ponds in Series w/ Tailwater (HEC-HMS)
- Example 5.10 Redevelopment I (Modified Rational Method)
- Example 5.11 Redevelopment II (Modified Rational Method)

## EXAMPLE 5.7 (SIMPLE)

- Determine the required detention volume for the 3-acre site shown below using the detention nomograph. It is assumed that the proposed site will provide the required volume control storage in the aggregate voids under the permeable pavement parking lot. It is also assumed there is no offsite tributary area or unrestricted flow area for the site.
  - 3-Acre site
  - CN = 89; impervious area
    = 1 acre
  - No offsite tributary area
  - No unrestricted releases
  - No tailwater conditions
  - Volume control storage = 1"



<u>Step 1</u>: Determine the required volume control storage for the site.

The Curve Number for the site is 89, with a total impervious area (open water and building) of 1 acre. The required volume control storage, V<sub>c</sub>, for the site is calculated as:

$$V_c = 1" \times \frac{1 \text{ foot}}{12 \text{ inches}} \times 1 \text{ acre} = 0.083 \text{ acre-feet}$$

<u>Step 2</u>: Determine the CN reduction corresponding to volume control calculated in Step 1.

Using the CN Adjustment Calculator spreadsheet, the adjusted curve number is 86.13 (it was assumed that only the required 1" of volume control storage would be provided).

RUNOFF CURVE NUMBER ADJUSTMENT CALCUL	ATOR				
Site Information:					
Total Site Area, A <sub>w</sub> (ac) =	3	]	Tota	l Impervious Area, A <sub>I</sub> (ac) =	1
Runoff R (in) =	6 28	-			
(iii) –	0.20				
P = rainfall depth (in) =	7.58				
CN =	89	]			
S =	1.24	]			
Runoff Volume Over Watershed V (ac-ft) =	1 57	1			
Ranon volume over watershea, v <sub>w</sub> (ac rt) =	1.57				
Volume of GI Provided:					
Control Volume V -	0.08	ac #	1" of volume		
control volume, v <sub>R</sub> –	0.08	ac-n	1 OI VOIUITE	over impervious area	
Additional Volume, V <sub>GI</sub> =	0.00	ac-ft	Additional v		
Adjusted Volume Over Watershed, $V_{ADJ} = V_{W} V_{R}$	. V <sub>GI</sub>				
V <sub>ADJ</sub> (ac-ft) =	1.49				
Adjusted Runoff Over Watershed R = V					
Augusteu nariori oter tratersneu) (Augusteu nariori	-				
R (in) =	5 94				
N <sub>ADJ</sub> (117) –	J.J <del>.</del>				
S <sub>adj</sub> =	1.61	_			
Adjusted CN for detention calcs, CN <sub>ADJ</sub> =	86.13				
*Riue values are entered by user	$\smile$				
brue values are entered by user					

<u>Step 3</u>: Using the adjusted CN determined in Step 2, use the detention nomograph from the TGM to determine the required detention volume.

0.23 acre-feet of detention volume is required for every acre of development, based on the adjusted CN of 86.13. By multiplying this value times the development area of 3 acres, the required detention volume is calculated to be 0.69 acre-feet.



\*Event hydrograph methods are still required to size overland flow routes in and out of detention basin

### EXAMPLE 5.8 (COMPLEX)

A proposed 5-acre commercial development has a curve number (CN) of 93 (80% impervious) and a time of concentration ( $t_c$ ) of 15 minutes. Based on Cook County one-foot topography, it was determined there are 3 acres of offsite tributary area to the project site. The offsite tributary area has a CN of 89 and a  $t_c$  of 12 minutes. The proposed development will provide the 1" of volume control storage in the void space of aggregate under a permeable parking lot. There is a 0.2-acre area with a CN of 74 and a  $t_c$  of 10 minutes that will release undetained from the site.

Determine the stormwater detention requirements for the site.

#### EXAMPLE 5.8 – PROBLEM OVERVIEW

• 5-acre site

Offsite tributary area = 3 acres

• Unrestricted area = 0.2 acres

No tailwater conditions

Volume control storage = 1"...

#### EXAMPLE 5.8 – PROBLEM OVERVIEW

Development Area = 5 acres (0.00781 square miles) CN = 93 (80% impervious area) T<sub>c</sub> = 15 minutes (Lag time = 9 minutes) Volume control storage provided = required 1"

Unrestricted Area = 0.2 acres (0.00031 square miles) CN = 74

Tc = 10 minutes (Lag time = 6 minutes)

Offsite Tributary Area = 3 acres (0.00469 square miles) CN = 89

Tc = 12 minutes (Lag time = 7.2 minutes)

<u>Step 1</u>: Determine the required volume control storage for the site.

The curve number for the site is 93, with a total impervious area of 4 acres. The required volume control storage,  $V_c$ , for the site is calculated as:

$$V_c = 1$$
" x  $\frac{1 \text{ foot}}{12 \text{ inches}}$  x 4 acres = 0.33 acre-feet

<u>Step 2</u>: Determine the CN reduction corresponding to volume control calculated in Step 1.

Using the CN Adjustment Calculator spreadsheet, the adjusted curve number is 86.22 (it was assumed that only the required 1" of volume control storage would be provided).

RUNOFF CURVE NUMBER ADJUSTMENT CALCUL	ATOR				
Site Information:					
Total Site Area, A <sub>w</sub> (ac) =	5		Tota	al Impervious Area, A <sub>I</sub> (ac) =	4
Runoff, R (in) =	6 75				
	0.70				
P = rainfall depth (in) =	7.58				
CN =	93				
S =	0.75	]			
Runoff Volume Over Watershed, V <sub>w</sub> (ac-ft) =	2.81	]			
Volume of GI Provided:					
Control Volume, V <sub>R</sub> =	0.33	ac-ft	1" of volume	e over impervious area	
Additional Volume, V <sub>GI</sub> =	0.00	ac-ft	Additional v	olume over the required 1"	
Adjusted Volume Over Watershed, V <sub>ADJ =</sub> V <sub>W</sub> . V <sub>R</sub>	. V <sub>GI</sub>				
V <sub>ADJ</sub> (ac-ft) =	2.48	]			
Adjusted Runoff Over Watershed, $R_{ADJ} = V_{ADJ}$	_				
Aw					
R <sub>ADJ</sub> (in) =	5.95				
S <sub>ADJ</sub> =	1.60	-			
Adjusted CN for detention calcs, CN <sub>ADJ</sub> =	86.22				
*Blue values are entered by user	$\smile$				

<u>Step 3</u>: Determine the allowable release rate for the site, accounting for the unrestricted area. The allowable release rate from the site is initially 1.5 cfs (0.3 cfs/acre x 5 acres) but should be adjusted to account for the 0.2-acre undetained area (which was delineated based on the proposed grading plan).

Net allowable release rate = maximum allowable release rate – unrestricted release rate

The unrestricted area must be modeled using HEC-HMS to determine the 100-year, 24-hour flowrate leaving the site

Set up HEC-HMS model to determine unrestricted release rate.

Create a new *Basin Model* to add the watershed components. In this case, there is one subbasin that represents the undetailed area of the project site (*Undetained*).

The *Meteorological Model* contains the rainfall depth information, which is the 100-year, 24-hour from Table 5-3 (7.58 inches). The *Time-Series Data* contains the time distribution of rainfall, which is the Huff 3<sup>rd</sup> quartile distribution for the 24-hour storm duration.

For Subbasin Undetained, enter the information : Area = 0.00031 square miles (0.2 acres) CN = 74Lag time = 6 minutes (0.6 \* t<sub>c</sub>) Specify SCS CN and Unit Hydrograph Methodology

Run the 100-year, 24-hour storm event to determine the unrestricted flowrate leaving the site.


Net allowable release rate = maximum allowable release rate – unrestricted release rate

Net allowable release rate = 1.5 cfs – 0.12 cfs = 1.38 cfs

0.30 cfs/acre \* site area

Unrestricted release rate

<u>Step 4</u>: Use the orifice equation spreadsheet to size the restrictor. Using the elevation-discharge spreadsheet, a 4.9-inch diameter restrictor is needed to pass the net allowable release rate of 1.38 cfs at the HWL of 605 ft.

ORIFIC	E/WEIR	STRUCT	URE RA	I ING AN	ALISIS							
BBB (507		Technical	deletere e Maria									
PROJECT	NAME:	Technical G	uidance ivian	uai								
PROJ. NO	.:	13-0409										
DESCRIPT	ION:	Example 5.7										
FILENAME	:	Orifice.xlsx										
DATE:		9-Feb-14										
		0.015105 ///										
OUTLET:		ORIFICE #1	4.86	IN. DIA. @	ELEV	600						
		ORIFICE #2	: N/A	IN. DIA. @	ELEV	N/A						
		WER #1:	N/A	FEETWID	E @ ELEV	N/A						
		WER #2:	N/A	FEET WID	E @ ELEV	N/A						
		ONE										
TURAUL	IC DIMENS	0145					1					
					#1	#2						
ORIFICE A	REA (ft <sup>2</sup> )				0.1288							
ORIFICE D	IAMETER (in	1)			4.9							
ORIFICE D	ISCHARGE	COEFFICIEN	<u>л</u>		0.61							
ORIFICE E	LEV. (ft-NAV	D88)			600.00							
TAILWATE	R OR CENT	ROID (ft-NAV	/D88)		600.20							
WEIR LEN	GTH (ft)											
WEIR COE	FFICIENT											
WEIR ELE	V. (ft-NGVD)											
					ORIFICE FLOW E	QUATION: Q = 0.6	A(2gH) <sup>0.5</sup>					
ELEVATIO	N-DISCHAR	GE RELATIO	ONSHIP		WEIR FLOW EQU	ATION: Q = 3.0L(H	f) <sup>1.5</sup>					
Elevation	Q-orifice #1	Q-orifice #2	Q-weir #1	Q-weir #2	Q-total							
(feet)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)		ORI	FICE RATIN	IG CURV	/E		
600.0	0.00	0.00	0.00	0.00	0.00	605.0						
600.5	0.34	0.00	0.00	0.00	0.34							
601.0	0.56	0.00	0.00	0.00	0.56	€04.0			_	ļ.,	$\square$	
601.5	0.72	0.00	0.00	0.00	0.72	ę						
602.0	0.85	0.00	0.00	0.00	0.85	<u></u> €03.0			_			
602.5	0.96	0.00	0.00	0.00	0.96	É				1		
603.0	1.05	0.00	0.00	0.00	1.05	G 602.0						
603.5	1.15	0.00	0.00	0.00	1.15	Ĕ						
604.0	1.23	0.00	0.00	0.00	1.23	601.0			-			
604.5	1.31	0.00	0.00	0.00	1.31	<b></b>						
605.0	1.38	0.00	0.00	0.00	1.38	600.0		0.0		10 12		
						°.	, uz 0.	0.6	0.8	1.0 1.2	1.4	
								DISCHARG	E (cfs)			
												-
						]						

Update the *Basin Model* to include the onsite area and proposed detention basin. In this case, there is one subbasin that represents the project site (Subbasin-1) and one storage area that represents the proposed detention pond (Reservoir-1).



Since the elevation-discharge relationship is fixed, the elevation-storage spreadsheet can be used to obtain the appropriate relationship to enter into HEC-HMS.

Using the elevation-storage spreadsheet, iteratively enter the elevation-storage relationship until the proposed basin fills up for the 100-year, 24-hour storm event. As shown in the figure to the right, a volume of 1.12 acre-feet is required for this site.

POND:	Propo	osed Detention F	acility	C	enterline Elevation	
JOB NO.		130409		Side Slopes	Orifice Radius:	
PROJECT:		Example 5.7		1	Orifice Coeff:	
FILE:		Storage.xls		4	Weir Elevation:	
DATE:		2/4/2014			Length of Weir	
DA					Weir Coeff	
		Are	a	Average	Incremental	Cummulative
Elevation	INC			Area	Storage	Storage
(ft)		(ft2)	(ac)	(ac)	(ac-ft)	(ac-ft)
600.00		6,080	0.140			
				0.155	0.15	
601.00		7,392	0.170			0.155
				0.186	0.19	
602.00		8,831	0.203			0.341
				0.221	0.22	
603.00		10,399	0.239			0.562
				0.258	0.26	
604.00		12,094	0.278			0.820
				0.299	0.30	
605.00		13,918	0.320			1.118

From the results of the HEC-HMS analysis for the 100-year, 24-hour storm event, the HWL of the proposed detention facility is 605.00 ft. Note the results indicate that the detention basin releases 1.38 cfs (net allowable release rate) at the HWL.



<u>Step 6</u>: Determine the 100-year peak flowrate (critical duration analysis) from offsite and onsite tributary areas to the detention facility to size emergency overflow weir.

A new subbasin (*Offsite*) is required to determine the peak flowrate of the offsite tributary area to the detention facility and a *junction* (*Junction-1*) is required to add the runoff hydrographs from the onsite and offsite tributary areas.



Critical Duration = 1-Hour Duration  $Q_{CRIT} = 37.7 \text{ cfs}$  $37.7 \text{ cfs} = 4.7 \text{ cfs/acre} > 1 \text{ cfs/acre} \rightarrow OK$ 

<u>Step 7</u>: Size the overflow weir to handle the peak 100-year flowrate to the detention facility.

 $\overline{Q} = C \times L \times H^{3/2}$ 

Where, Q = flowrate (37.7 cfs) C = weir coefficient (assume 3.0) L = length of weir (ft) H = head on weir (ft, assume 1 ft)

Solving for L,

L = 12.6 ft, which is the minimum length of weir required to pass the 100-year peak flowrate (with one foot of head) for the onsite and offsite area.

# EXAMPLE 5.9 – PONDS IN SERIES W/ TAILWATER

As shown in the figure below, the required detention volume for a proposed 10acre commercial development will be provided in two detention basins in series. Based on Cook County one-foot topography, there is no offsite tributary area to the project site. However, Detention Basin 2 will discharge to a receiving stream with a 100-year flood elevation of 699 ft. Based on the proposed grading plan, the site is separated into two subbasins.

Determine the requirements of the two detention basins based on the WMO and TGM.



# EXAMPLE 5.9 – PROBLEM OVERVIEW

- 10-acre site
- Two detention ponds in series
- No offsite tributary area
- No unrestricted releases
- Tailwater (100-year) = 699 ft
- Volume control storage = 1".

#### EXAMPLE 5.9 – PROBLEM SUMMARY

Subbasin 1 Area = 0.009375 square miles (6 acres) Impervious Area = 2.25 acres Curve Number = 92 Adjusted Curve Number = 88.79 (assumes 1" on volume control storage) SCS Lag Time = 9 minutes

<u>Subbasin 2</u> Area = 0.00625 square miles (4 acres) Impervious Area = 1.25 acres Curve Number = 88 Adjusted Curve Number = 85.36 (assumes 1" on volume control storage) SCS Lag Time = 6 minutes

#### EXAMPLE 5.9 – PROBLEM SUMMARY, CONT.

<u>Detention Basin 1 (Reservoir-1)</u> Normal Water Level (NWL) = 700 ft High Water Level (HWL) = 704 ft Tailwater Condition = none

Detention Basin 2 (Reservoir-2) Normal Water Level (NWL) = 698 ft High Water Level (HWL) = 702 ft Tailwater Condition = 699 ft (100-year flood elevation of receiving stream)



<u>Step 1</u>: Set up a HEC-HMS model for the project. As shown below, Subbasin-1 drains to Reservoir-1, and the outflow of Reservoir-1 then drains into Reservoir-2, along with Subbasin-2.



<u>Step 2</u>: Since the configuration of *Reservoir-2* depends on the outflow from *Reservoir-1*, *Reservoir-1* must be configured first.

It should be noted that as long as the release rate at the site's outlet (*Reservoir-2* outflow) is less than or equal to 3 cfs (0.30 cfs/acre x 10 acres), the proposed detention configuration is flexible. For example, if site conditions prevent *Reservoir-1* from detaining *Subbasin-1* at 0.30 cfs/acre, *Reservoir-1* can be sized to underdetain its tributary area, so long as *Reservoir-2* is oversized to meet the allowable release rate for the site.

In this example, it is assumed that *Reservoir-1* can be sized to detain its onsite tributary at the allowable release rate of 0.30 cfs/acre.

<u>Step 2</u>: Determine the orifice size necessary to release 1.80 cfs (0.30 cfs/acre x 6 acres) at the HWL of Reservoir-1.

From the orifice equation spreadsheet (shown to the right), a 5.9-inch diameter restrictor is needed to convey 1.8 cfs at the HWL of 704 ft.

PROPO	SED CO	NDITION	S											
		SIRUCI			AL 1313									
PROJECT	NAME:	Example 5.9												
PROJ. NO.	:	13-0409												
DESCRIPT	ION:	Detention Ba	ISIN 1											
FILENAME		Orifice.xlsx												
DATE:		9-Feb-14												
OUTLET:		ORIFICE #1:	5.9	IN. DIA. @	ELEV	700								
		ORIFICE #2:	N/A	IN. DIA. @	ELEV	N/A								
		WEIR #1:	N/A	FEET WID	E @ ELEV	N/A								
		WEIR #2:	N/A	FEET WID	E @ ELEV	N/A								
HYDRAULI	C DIMENSI	ONS												
					# 1		#2							
	REA (ft <sup>2</sup> )				0.1899									
ORIFICE DI	IAMETER (ir	1)			5.9									
ORIFICE DI	ISCHARGE	COEFFICIEN	Т		0.61									
ORIFICE EI	LEV. (ft-NAV	D88)			700.00									
TAILWATER	R OR CENT	ROID (ft-NAV	D88)		700.25									
WEIR LENG	GTH (ft)	ĺ												
WEIR COE	FFICIENT													
WEIR ELE	/. (ft-NGVD)													
					ORIFICE FLOW FC		N Q = 0.6A	(2aH) <sup>0.5</sup>						
ELEVATIO	N-DISCHAR	GE RELATIO	ONSHIP		WEIR FLOW EQU	ATION:	Q = 3.0L(H)	1.5						
Elevation	O-orifice #1	O-orifice #2	O-weir #1	O-weir #2	O-total	i (								
(feet)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)			0	RIFICE	RATING CU	RVE			
700.0	0.00	0.00	0.00	0.00	0.00		704.0	-				_		
700.0	0.00	0.00	0.00	0.00	0.00								-	
701.0	0.47	0.00	0.00	0.00	0.47									
701.5	1.04	0.00	0.00	0.00	1 04		88 703.0				/			
702.0	1.34	0.00	0.00	0.00	1.04									
702.5	1.20	0.00	0.00	0.00	1.20		2 702.0							
703.0	1.54	0.00	0.00	0.00	1.54		E 7							
703.5	1.68	0.00	0.00	0.00	1.64		Q 701.0							
704.0	1.80	0.00	0.00	0.00	1.80		LA/							
	1.00	0.00	0.00	0.00	1.00		É .							
							U 700.0	0.0 0.2 0.4	0.6	0.8 1.0 1.2	1.4 1.6	1.8 2.0		
									DIS	CHARGE (cfs)				
						i (			510					
						1								

<u>Step 3</u>: Determine the stage-storage relationship so that *Reservoir-1* fills up for the 100-year, 24-hour storm event.

Using the elevationstorage spreadsheet and solving iteratively, it is determined that 1.40 acre-feet of storage volume is required for *Reservoir-1*.



<u>Step 3</u>: Size the restrictor for Reservoir-2 so that it releases 3.0 cfs at the HWL assuming full release conditions. As shown on the next slide, a 7.7-inch diameter restrictor is needed to convey the allowable release rate.

However, since there is a tailwater condition on this restrictor, the detention volume must be sized assuming the 100-year tailwater of the receiving stream (699 ft). Therefore, another stage-discharge spreadsheet needs to be developed to determine the outflow assuming the 100-year tailwater of 699 ft. This relationship will be used as the input to HEC-HMS to determine the required volume.

PROPO	SED CO	NDITION	s									
ORIFICE	E/WEIR	STRUCT	JRE RAT	TING AN	ALYSIS							
PROJECT	NAME:	Example 5.9										
PROJ. NO.	.:	13-0409										
DESCRIPT	'ION:	Detention Ba	isin 2									
FILENAME	:	Orifice.xlsx										
DATE:		9-Feb-14										
OUTLET:		ORIFICE #1:	7.65	IN. DIA. @	ELEV	698						
		ORIFICE #2:	N/A	IN. DIA. @	ELEV	N/A						
		WEIR #1:	N/A	FEET WID	E @ ELEV	N/A						
		WEIR #2:	N/A	FEET WID	E @ ELEV	N/A						
HYDRAULI	IC DIMENSI	ONS										
					# 1	#2						
ORIFICE AF	REA (ft <sup>2</sup> )				0.3192							
ORIFICE D	IAMETER (ir	1)			7.7							
ORIFICE D	ISCHARGE	COEFFICIEN	т		0.61							
ORIFICE EI	LEV. (ft-NAV	D88)			698.00							
TAILWATER	R OR CENT	ROID (ft-NAV	D88)		698.32							
WEIR LENG	GTH (ft)											
WEIR COE	FFICIENT											
WEIR ELE\	V. (ft-NGVD)											
					ORIFICE FLOW ED	QUATION: Q = 0.6A	(2gH) <sup>0.5</sup>					
ELEVATIO	N-DISCHAR	GE RELATIO	ONSHIP		WEIR FLOW EQU	ATION: Q = 3.0L(H)	1.5					
Elevation	Q-orifice #1	Q-orifice #2	Q-weir #1	Q-weir #2	Q-total							
(feet)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)		ORI	FICE RA	TING CUF	RVE		
698.0	0.00	0.00	0.00	0.00	0.00	702.0						
698.5	0.67	0.00	0.00	0.00	0.67			1				
699.0	1.29	0.00	0.00	0.00	1.29	- 701.0						
699.5	1.70	0.00	0.00	0.00	1.70	8 B						
700.0	2.03	0.00	0.00	0.00	2.03	A						
700.5	2.31	0.00	0.00	0.00	2.31	Z 700.0 ∉			- /			
701.0	2.56	0.00	0.00	0.00	2.56	z		1				
701.5	2.79	0.00	0.00	0.00	2.79	₽ eso.o		-	$\frown$			
702.0	3.00	0.00	0.00	0.00	3.00	_ ×		1				
						H 08.0		1				
						0.0	0.5	1.0	1.5	2.0 2.5	3.0	
								DISCH	ARGE (cfs)			]
												-

Restrictor for *Reservoir-2* (no tailwater) (used for design)

			<u>^</u>								1				
РКОРО	SED CO	NDITION	5												
ORIFIC	E/WEIR	STRUCTI	JRE RA	ting an	ALYSIS										
PROJECT	NAME:	Example 5.9													
PROJ. NO	:	13-0409													
DESCRIPT	ION:	Detention Ba	isin 2												
FILENAME		Orifice.xlsx													
		9-Feb-14													
		010011													
		ORIFICE #1	7 65	IN DIA @	FLEV	698									
OUTLET.		ORIFICE #2	N/A	IN DIA @	FLEV	Ν/Δ									
		WEID #1.	N/A	EEET WID		NI/A									
		WEIR #1.	N/A	EEET WID		NI/A									
		WEIN #2.	19/7			IN/A									
		0110													
HIDRAUL	IC DIMENSI	UNS				-									
					#1		#2								
ORIFICE A	REA (ft <sup>2</sup> )				0.3192										
ORIFICE D	IAMETER (ir	1)			7.7										
ORIFICE D	ISCHARGE	COEFFICIEN	Т		0.61										
ORIFICE E	LEV. (ft-NAV	D88)			698.00										
TAILWATE	R OR CENT	ROID (ft-NAV	D88)		699.00										
WEIR LEN	GTH (ft)					T									
WEIR COE	FFICIENT														
WEIR ELE	V. (ft-NGVD)														
	ĺ				1										
					ORIFICE FLOW F	OLIATK	ON' O = 0.6	(2nH) <sup>0.5</sup>							
ELEVATIO	N-DISCHAR	GE RELATIO	ONSHIP		WEIR FLOW EQU	JATION:	Q = 3.0L(H	1.5							
Elevation	Q-orifice #1	Q-orifice #2	O-weir #1	O-weir #2	Q-total	1 (									
(feet)	(cfs)	(cfs)	(cfs)	(cfs)	(cfs)				OR	FICE			VE		
698.0	0.00	0.00	0.00	0.00	0.00				011			0.001			
698.5	0.00	0.00	0.00	0.00	0.00		/02.0								
600.0	0.00	0.00	0.00	0.00	0.00								/	1	
600.5	1 10	0.00	0.00	0.00	1.10										
700.0	1.10	0.00	0.00	0.00	1.10		ä								
700.0	1.00	0.00	0.00	0.00	1.00		₹					/			
700.5	1.91	0.00	0.00	0.00	1.91		2 700.0				$\geq$	·			1
701.0	2.21	0.00	0.00	0.00	2.21	-	Z								
701.5	2.4/	0.00	0.00	0.00	2.4/		E 609.0						_		
702.0	2.71	0.00	0.00	0.00	2.71		× ×								
							698.0	.0 (	1.5	1.0	1.6	5	2.0	2.5	3.0
										DIS	HARG	E (cfs)			
										0101		- (010)			)

Restrictor for *Reservoir-2* (tailwater = 699 ft) (used to size detention volume)

Using the elevation-storage spreadsheet and solving iteratively, it is determined that 1.30 acre-feet of storage volume is required for *Reservoir-2*, which allows the basin to fill up to its HWL of 702 ft and release at the allowable release rate. Note that when there is a 100-year tailwater on the detention basin, the release rate is only 2.7 cfs. When there is no tailwater condition, the outflow of the detention basin will be no greater than the maximum allowable release rate of 3.0 cfs.

POND:	Propos	sed Detention Fa	acility 2	C	enterline Elevation		😕 Basin Model [Basin 1] Current Run [100YR24HR]
JOB NO.		130409		Side Slopes	Orifice Radius:		×
PROJECT:		Example 5.7		1	Orifice Coeff:		
FILE:		Storage.xls		4	Weir Elevation:		
DATE:		2/10/2014			Length of Weir		🚔 Subbasin-1 🚔 Subbasin-2
DA					Weir Coeff		
							Reservoir-1
		Ar	ea	Average	Incremental	Cummulative	
Elevation	INC			Area	Storage	Storage	Reservoir-2
(ft)	0.25	(ft2)	(ac)	(ac)	(ac-ft)	(ac-ft)	📰 Summary Results for Reservoir "Reservoir-2"
							Project: Example5.9
698.00		10,522	0.242				Simulation Run: 100YR24HR Reservoir: Reservoir-2
				0.261	0.26		Start of Run: 01Jan2000, 00:00 Basin Model: Basin 1 End of Run: 03Jan2000, 00:00 Meteorologic Model: 100YR24HR
699.00		12,228	0.281			0.261	Compute Time: 10Feb2014, 16:14:02 Control Specifications: 24HR
				0.302	0.30		Volume Units: <ul> <li>IN</li> <li>AC-FT</li> </ul>
700.00		14,061	0.323			0.563	Computed Results
				0.345	0.35		Peak Innow : 4.50 (CFS) Date/Time of Peak Inflow : 01Jan2000, 15:00 Peak Outflow : 2.71 (CFS) Date/Time of Peak Outflow : 01Jan2000, 19:03
701.00		16,022	0.368			0.908	Total Inflow : 6.082 (IN) Peak Storage : 1.30 (AC-FT) Total Outflow : 5.760 (IN) Peak Elevation : 702.00 (FT)
				0.392	0.39		
702.00		18,112	0.416			1.300	

# EXAMPLE 5.10 - REDEVELOPMENT

An existing 11.3-acre industrial area is to be redeveloped into a shopping mall. The original development contains a detention facility that was permitted under the Sewer Permit Ordinance (SPO). The proposed development has a C value of 0.90, with 8.0 acres of impervious area. It is assumed that the proposed development will provide the 1" of volume control storage. Determine the required detention volume for the site.

# EXAMPLE 5.10 – PROBLEM OVERVIEW

- 11.33-acre site
- Onsite detention facility permitted under SPO
- No known drainage problems associated with upstream drainage area
- Allowable release rate = previously permitted (Schedule D)
- No tailwater conditions
- Volume control storage = 1"

<u>Step 1</u>: Obtain the Schedule D form for the original development to determine the composite runoff coefficient (C value) and required detention volume that was permitted. As shown on Page 2 of the Schedule D form, the permitted development in this example has a C value of 0.88 and a required detention volume of 3.07 acre-feet.

		0	~
SCHE	DULE D – DETENTION	MWRDGC Permit No.	
A. I	PROJECT INFORMATION		°C2
	Name of Project	(as shown on plans)	- Qâ
B. 7	METHOD OF DETENTION:		
0	Reservoir 🗌 Rooftop 🗌 Parking I	Lot Others_	
C. 1	JNDEVELOPED SITE_DETERMINATIO	ON OF ALLWABLE RELEAS d areas on a grading plan)	SE (Delineate
	1. Area of Site	11.334	ficres .
	2. Average Ground Slope	0.0024	feet/foot
	<ol> <li>Longest overland flow distance (Shown on a contour map for undeveloped site)</li> </ol>	1250	feet
	4. Overland flow time of concentration	97	minutes
	<ol> <li>Average slope of channelized flow (see note)</li> </ol>		feet/foot
	6. Channelized flow distance (see note)	· · · · · · · · · · · · · · · · · · ·	feet
	7. Channelized flow time of concentration	-	minutes
	8. Total time of concentration (time 4 + line 7)	97	minutes
	9. Rainfall intensity for 3- year storm	1.21	inches/hr.
	10. Gross Allowable release rate (0.15 x line 9 x line 1 or Q <sub>st</sub> =0.15 x i <sub>3</sub> x A)	2.057.	cfs
	11. Unrestricted release rate $(Q_{un})$ $Q_{un} = C_{un}(i_{un-100})(A_{un})$	0.874	cfs
	12. Net allowable rolease rate (line 10 - line 11)	1.183	cfs
	13. Actual release rate at HWL 594.00-Fr (must be less than or equal to line 12)	1.183 (H.W.=594.00)	cfs
	<ol> <li>Restrictor type and size / N V = 580.%</li> <li>(provide details and calculations)</li> </ol>	-f4 4.47 (H.W.=594.00)	inches

			-	
SCI	IEDUI	LE D – DETENTION MW	RDGC Permit No	111
D.	DEVI (Subn	LOPED SITE-DETERMINATION OF nit calculations for Items 1 through 6)	RESERVOIR SIZE	"CO
	1.	Impervious drainage area excluding wet	9.431	acres 4
	2.	Impervious wet pond area1	0.965	acres
	3.	Pervious drainage area <sup>1</sup>	0.796	acres
	4.	Composite runoff coefficient (C)	0.88	
	5.	Required detention capacity provided at	3.07 (H.W.=(593.98)	acre-feet
	6.	Actual detention capacity provided at HWL	3.084 (H.W.=594.00)	acre-feet
1 Unre	stricted are	574.0077 as shall be excluded here.		
E.	REQU	(0.115 - AL IMPERVICUS I JIRED BYPASS RATE THROUGH DE REAM AREA	NO 0.027 - AC VELOPMENT SITE FROM	NERNAUS,
Note: freque freque	Followin ency shall ency. (De	g steps are applicable to bypass flow over a wei be determined by local ordinance. If no local re lineate bypass areas on grading plans or USGS re	r or bypassing detention system quirement is established, use 5- maps).	n. Design -year storm
Note: freque freque	Followin ency shall ency. (De 1.	g steps are applicable to bypass flow over a wei be determined by local ordinance. If no local re lineate bypass areas on grading plans or USGS i Total area upstream	r or bypassing detention system equirement is established, use 5- maps). N/A	n. Design -year storm acres
Note: freque freque	Followin ency shall ency. (De 1. 2.	g steps are applicable to bypass flow over a wei be determined by local ordinance. If no local re lineate bypass areas on grading plans or USGS i Total area upstream Impervious area	r or bypassing detention system equirement is established, use 5- maps). N/A	<ul> <li>Design -year storm acres acres</li> </ul>
Note: freque freque	Followin ency shall ency. (De 1. 2. 3.	g steps are applicable to bypass flow over a wei be determined by local ordinance. If no local re lineate bypass areas on grading plans or USGS i Total area upstream Impervious area Pervious area	r or bypassing detention system equirement is established, use 5- nape). N/A	<ul> <li>Design         -year storm         acres         acrecres         acrecre         acres         acres         acrec</li></ul>
Note: freque freque	Followin mcy shall ency. (De 1. 2. 3. 4.	g steps are applicable to bypass flow over a wei be determined by local ortinance. If no local its limitate bypass areas on grading plans or USGS it Total area upstream Impervious area. Pervious area. Composite runoff coefficient (minimum of 3.5)	r or bypassing detention system quitement is established, use 5- maps). N/A	<ul> <li>Design         -year storm         acres         acres         acres         acres         .</li> </ul>
Note: freque freque	Followin mcy shall ency. (De 1. 2. 3. 4. 5.	g steps are applicable to bypass flow over a wei be determined by local ordinance. If no local re lineate bypass areas on grading plans or USOS i Total area upstream Impervious area Pervious area Composite runoff coefficient (minimum of 0.35) Design storm frequency for the upstream area	r or bypassing detention system equirement is established, use 5- N/A	1. Design -year storm acres acres year
Note:	Followin ency shall ency. (De 1. 2. 3. 4. 5. 6.	g steps are applicable to bypass flow over a wei be determined by local ordinance. If no local is limited bypass areas on grading plans or USGS in Total area upstream Impervious area. Pervious area. Composite runoff coefficient (minimum of 0.35) Design storm frequency for the upstream area. Time oncentration for upstream area at point of entry, upstream area to be considered as Security plant.	r er bypassing detention system oquivennen is established use 5 NAA	1. Design -year storm acres acres acres year minutes
Note:	Followin ency shall ency. (De 1. 2. 3. 4. 5. 6. 7.	g steps are applicable to bypass flow over a wei be determined by local ordinance. If no local to lineate bypass areas on grading plans or USG's Total area upstream Impervious area. Pervious area. Composite runoff coefficient (minimum of 0.35) Design aftern frequency for the upstream area. Time oncentration for upstream area at point of entry, upstream area to be considered as declapted Rainfall intensity for time of concentration	r cr bypassing detuntion system opplimment is established use 5 	1. Design -year storm acres acres acres year minutes inches/hr.
Note: freque	Followin mcy shall ency. (De 1. 2. 3. 4. 5. 6. 7. 8.	g steps are applicable to bypass flow over a wei be determined by local ordinance. If no local to finate bypass areas on grading plans or USO'S i Total area upstream Impervious area Pervious area Pervious area Compassion runoff exeficient (minimum of 0.35) Design atom frequency for the upstream area Time consentration for upstream area at point of entry, upstream area to be considered as <u>desible</u> ptd Rainfall intensity for time of concentration Permissible bypass rate (fine 1 x line 4 x line 7)	r or bypassing detention system quierement in established, use 5 	s. Design acres acres acres year minutes inches/hr. cfs
Note: freque	Followin mcy shall ency. (De 1. 2. 3. 4. 5. 6. 7. 8. 9.	g steps are applicable to bypass flow over a wei be determined by local ordinance. If no local to finate bypass areas on grading plans or USOS i Total area upstream Impervious area Pervious area Pervious area Compassion runoff csefficient (minimum of 0.35) Design atoms frequency for the upstream area Time consentration for upstream area at point of airty upstream area to be considered as <u>desibled</u> Rainfall intensity for time of concentration Permissible bypass rate (line 1 x line 4 k line 7) Dypass system — Type & capacity (provide detail up and ealoukation)	r or bypassing detention system quierement in established, use 5 	s. Design sores acres acres year minutes inchente. efs cfs
Note: freque freque	Followin mcy shall ency. (De 1. 2. 3. 4. 5. 6. 7. 8. 9. 3.	g steps are applicable to bypass flow over a wei be determined by local ordinance. If no local to lineate bypass areas on grading plans or USOS i Total area upstream Impervious area Pervious area Composite ranoff coefficient (mintum of 0.35) Design storm frequency for the upstream area Time concentration for upstream area at point of entry upstream area to be comindered as <u>desible</u> ptd Rainfall intensity for time of concentration Permissible bypass rate (into 1 xin de x line 7) Bypass system — Type & capacity (provide detail and calculation)	r or bypassing detention system quierenen in established, use 5 N/A	s. Design sores acres acres year minutes incheaftr. efs cfs

Page 2 of 2

<u>Step 2</u>: Determine if the redevelopment can meet the conditions for detention allowances provided in Section §505.3 of the WMO. The four conditions are:

- Design of the existing detention facility is documented and approved under an existing sewerage system permit;
- The actual storage volume is verified to meet the required permitted volume (3.07 acre-feet in this example) by a survey;
- The redevelopment will meet the volume control requirements of the WMO; and
- The redevelopment provides adequate conveyance to convey the 100-year peak flowrates to the detention facility.

<u>Step 3</u>: Assuming the redevelopment can meet the four conditions outlined in the previous slide, calculate the redevelopment's C value.

Using the values provided in Table 5-2 of the TGM, the redeveloped C value is 0.90. Because the redeveloped C value (0.90) is greater than existing (0.88), additional detention storage is required.

<u>Note</u>: If the redeveloped C value matched the permitted C value of 0.88, no additional storage volume would be required.

<u>Step 4</u>: Determine the required storage volume for the redevelopment using the modified rational method and Bulletin 70 rainfall depths. Since the existing detention facility was previously permitted under the SPO, the original release rate and restrictor can be used. From Page 1 of the Schedule D form, the allowable release rate is 1.183 cfs.

The required detention volume for the redevelopment is 4.44 ac-ft. Since the provided detention storage for the original development was 3.08 ac-ft, the additional storage that is required is 1.36 acre-feet. The provided volume control storage (0.67 ac-ft) is credited toward this total, therefore only 0.69 ac-ft of additional detention volume is required.

#### DETENTION STORAGE CALCULATIONS

(Bulletin 70 NE Sectional Rainfall Intensities)

PROJECT:	Example 5.10				
JOB NO.:	Technical Guida	nce Manual			
FILENAME:	ModRatB70.xls>	(			
DATE :	5-Feb-14				
	TRIBUTARY AR	EA =		11.33	acres
	COMPOSITE R	UNOFF COEFFI	CIENT =	0.90	
	ALLOWABLE R	ELEASE RATE	=	1.18	cfs
	COMPL	JTED DETENTIO	N STORAGE =	4.441	acre-ft
		RAINFALL	INFLOW	STORED	RESERVOIR
DURATION	TIME	INTENSITY	RATE	RATE	SIZE
(hours)	(min.)	(in/hr)	(cfs)	(cfs)	(ac-ft)
0.08	5	10.90	111.19	110.01	0.758
0.17	10	10.02	102.21	101.03	1.392
0.25	15	8.20	83.64	82.46	1.704
0.33	20	7.30	74.46	73.28	2.019
0.50	30	5.60	57.12	55.94	2.311
0.67	40	4.58	46.72	45.54	2.509
0.83	50	3.97	40.50	39.32	2.708
1	60	3.56	36.31	35.13	2.903
1.5	90	2.68	27.34	26.16	3.243
2	120	2.24	22.85	21.67	3.581
3	180	1.62	16.52	15.34	3.803
4	240	1.40	14.28	13.10	4.330
5	300	1.17	11.93	10.75	4.441 🗲
6	360	0.95	9.69	8.51	4.218
7	420	0.83	8.47	7.29	4.216
8	480	0.75	7.65	6.47	4.276
9	540	0.68	6.94	5.76	4.282
10	600	0.63	6.43	5.25	4.336
11	660	0.59	6.02	4.84	4.397
12	720	0.55	5.61	4.43	4.390
18	1080	0.39	3.98	2.80	4.161
24	1440	0.32	3.26	2.08	4.120
36	2160	0.22	2.24	1.06	3.145
48	2880	0.17	1.73	0.55	2.170
<b>4</b>	1				

# EXAMPLE 5.10 – ADDITIONAL NOTES

- The allowable release rate calculated for the original development included unrestricted releases; if the redevelopment causes additional unrestricted releases, or if the applicant wants to use a larger release rate because unrestricted areas have been reduced, a modification to the outlet control structure would be required.
- The overflow weir for the detention facility may need to be retrofitted to meet the design requirements of the WMO if there is a known drainage problem associated with the upstream drainage area to the development.

# EXAMPLE 5.11 - REDEVELOPMENT

For the site in Example 5.10, determine the required detention volume if only a 6-acre portion of the site is to be redeveloped.



<u>Step 1</u>: Calculate the proposed C value of entire development,  $C_{REDEV}$ , which includes redeveloped parcel. If  $C_{REDEV}$  > permitted C value for the development,  $C_{PERMIT}$ , additional storage volume is required.

C<sub>PERMIT</sub> = 0.88 (from Schedule D form for original development) C<sub>REDEV</sub> = 0.89 (entire development including redeveloped 6-acre parcel)

Since  $C_{REDEV} > C_{PERMIT}$ , additional storage volume is required.

<u>Step 2</u>: Determine the pro-rated <u>permitted</u> detention volume for the 6-acre parcel.

From the Schedule D for the original development, 3.07 acre-feet is required for the 11.33 acre-feet development. The pro-rated detention volume for the 6-acre parcel is:

 $\frac{V_{PERMIT}}{A_{PERMIT}} \times A_{PARCEL} = Permitted Storage Volume Allocated for Redeveloped Parcel$  $<math display="block">\frac{3.07 \text{ acre-feet}}{11.33 \text{ acres}} \times 6 \text{ acres} = 1.63 \text{ acre-feet}$ 

<u>Step 3</u>: Using the modified Rational Method w/ Bulletin 70 rainfall depths, determine the pro-rated <u>required</u> detention volume for the 6-acre parcel.



PROJECT:	Example 5.10						
IOB NO.:	Technical Guida	nce Manual					
FILENAME:	ModRatB70.xls>	(					
DATE:	5-Feb-14						
	TRIBUTARY AR	EA =		11.33	acres		
	COMPOSITE R	JNOFF COEFFI	CIENT =	0.89			
	ALLOWABLE R	ELEASE RATE	=	1.18	cfs		
	COMPL	JTED DETENTIO	N STORAGE =	4.387	acre-ft		
		RAINFALL	INFLOW	STORED	RESERVOIR		
DURATION	TIME	INTENSITY	RATE	RATE	SIZE		
(hours)	(min.)	(in/hr)	(cfs)	(cfs)	(ac-ft)		
0.08	5	10.90	109.91	108.73	0.749		
0.17	10	10.02	101.04	99.86	1.375		
0.25	15	8.20	82.69	81.51	1.684		
0.33	20	7.30	73.61	72.43	1.995		
0.50	30	5.60	56.47	55.29	2.285		
0.67	40	4.58	46.18	45.00	2.479		
0.83	50	3.97	40.03	38.85	2.675		
1	60	3.56	35.90	34.72	2.869		
1.5	90	2.68	27.02	25.84	3.203		
2	120	2.24	22.59	21.41	3.538		
3	180	1.62	16.34	15.16	3.758		
4	240	1.40	14.12	12.94	4.277		
5	300	1.17	11.80	10.62	4.387 🗲		
6	360	0.95	9.58	8.40	4.164		
7	420	0.83	8.37	7.19	4.158		
8	480	0.75	7.56	6.38	4.216		
9	540	0.68	6.86	5.68	4.223		
10	600	0.63	6.35	5.17	4.270		
11	660	0.59	5.95	4.77	4.334		
12	720	0.55	5.55	4.37	4.331		
18	1080	0.39	3.93	2.75	4.086		
24	1440	0.32	3.23	2.05	4.060		
36	2160	0.22	2.22	1.04	3.085		
48	2880	0.17	1.71	0.53	2.091		

(Bulletin 70 NE Sectional Rainfall Intensities)

<u>Step 4</u>: Determine the additional storage volume required.

Additional Storage Volume required =  $V_{REDEV} - V_{PERMIT}$ 

Additional Storage Volume required = 2.32 ac-ft – 1.63 ac-ft

Additional Storage Volume required = 0.69 ac-ft

Since additional storage volume required > 0.10 ac-ft and is not within 2% of the existing volume, the additional storage volume must be provided. Assuming 0.45 ac-ft of volume control storage was provided as part of the redevelopment of the parcel, the net volume that is required is 0.24 ac-ft.